

ANALYTICAL EFFECTIVE METHOD FOR VERIFICATION OF A SATELLITE PASS OVER A REGION OF THE EARTH SURFACE

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Abstract

An analytical method is proposed in this work for verification whether an artificial earth satellite during its orbital motion passes over a region of the earth surface. The method is based on undisturbed Kepler's approximation of the orbit and approximation of the region by a circular segment S . In order to define the situational condition, a conic surface is used with apex in the earth centre, cutting out the circular segment. The tangents of the conical surface with Kepler's plane determine the time intervals in which the satellite trace on the earth surface occurs inside the segment S . The transformation of these tangents in the plane of Kepler's orbit and the determination of their crossing points with Kepler's ellipse lies in the basis of the examined method.

1. Introduction.

A number of cases exist when, during space experiments, it is necessary to know the time of a satellite pass over a definite region of the earth surface. Thus, for example, in synchronous satellite and ground-based measurements, it is important when the satellite passes over a definite territory where the ground-based station is located. When problems of meteorological character are solved on the basis of satellite information, it is significant when the satellite is going to pass over a definite territory or a meteorological structure (cyclone centre, front). The solution of many other problems, connected with the study of the earth surface from space is connected with the determination of the temporal interval pass over a specific region. This is necessary in some of the cases for experiments

planning. In other cases, the analysis is needed to schedule the scances for receiving satellite information. In both cases this is important for the quality of the conducted experiments, and from economical point of view.

The problem for determining a satellite pass over a definite geographic region has a standard solution. It is obtained on the basis of the imitation modelling by selecting a proper geometrical model for region V which determines the situational condition. The discretization of the solution of the artificial earth satellite motion equation and the respective analysis, as concerns the model of the region, allow to determine whether the satellite passes over the region as well as the moments of crossing its borders.

For the equation of the artificial earth satellite motion in geocentrical co-ordinate system (GcCS) we have:

$$(1) \quad m \frac{d^2 \vec{r}}{dt^2} = -\sum \vec{f}_k,$$

with initial conditions $\vec{r}_0 = \vec{r}(t_0)$, $\frac{d\vec{r}}{dt} = \frac{d\vec{r}(t_0)}{dt}$, where \vec{r} is the satellite radius-vector; m - its mass and t - the time. The specific form of (1) reflects the accepted motion model. The solution of (1) can be obtained on the basis of analytical or numerical methods [1,2]. In any case, a discretization of the solution of (1) is obtained:

$$(2) \quad \vec{r}_{t_0}, \vec{r}_{t_1}, \vec{r}_{t_2}, \dots, \vec{r}_{t_n}, \dots$$

Usually (2) is obtained in GcCS or in orbital co-ordinate system (OCS). It is necessary to transform the solution of (1) into Greenwich co-ordinate system (GrCS):

$$(3) \quad \vec{r}_{(GrCS)} = \alpha_{GrG} \cdot \vec{r}_{(GcCS)}$$

In (3) α_{GrG} is the transformation matrix [3].

Problems exist in which region V is restricted by a complex outline contour (for example, a state border). There are known methods to present V and to solve the problem for crossing its borders by the sub-satellite trace [4]. Within the terms of different problems, the approximation of region V by a circular spherical segment of the earth surface is completely sufficient and substantiated both physically and of geometrical point of view. The

application of such a simplifying situational condition in the discretization of the solution of the artificial earth satellite motion equation requires also considerable computation time.

The verification of the situational condition is made by a step in the time Δt and even within one satellite circle it is connected with a multiple repetition of the respective computation procedure. It is connected with considerable computational expenses. This paper suggests an analytical method to apply the verification procedure once for a whole period of the satellite circle.

2. Formulation of the Problem.

We shall examine the considered region of the earth surface as a spherical segment S (Fig. 1). It is cut out of the earth surface by a straight circular cone with angle ψ between the axis and the generant and its apex is in the earth centre. The crossing point of the cone axis with the earth surface has Greenwich co-ordinates (λ, Θ) . Therefore, the segment can be described by the following parameters – angle ψ , earth radius R_{\oplus} and the Greenwich co-ordinates λ and Θ , i.e. $S(\psi, R_{\oplus}, \lambda, \Theta)$. Moving along with the earth surface, the cone tangents with the plane of Kepler's orbit at its two sides at moments t_1 and t_2 . (Fig. 2). Between the two moments t_1 and t_2 , the Kepler's plane and the conic surface intercross. This means that part of the Kepler's ellipsis is also restricted within the limits of the conic surface and that it is located over segment S .

We shall discuss an approach, allowing to obtain moments \tilde{t}_1 and \tilde{t}_2 when the satellite crosses the cone generants $\vec{\tau}_1$ and $\vec{\tau}_2$ which tangent with the Kepler's orbit.

The relation between the intervals (t_1, t_2) and $(\tilde{t}_1, \tilde{t}_2)$ on the time axis shows whether the artificial earth satellite passes over segment S (Fig. 3). If the two intervals intercross, then the condition for passing over the examined segment is fulfilled.

3. Construction of an algorithm.

Let's assume that segment S forms a tangent with K . For distance δ from the centre of S to K we can write down [5]:

$$(4) \quad \frac{\vec{n}}{|\vec{n}|} (\vec{R}_c \times \vec{x}) = \delta = \sin \psi \cdot R_{\oplus}$$

or

$$(4') \quad \vec{n}^0 \cdot \vec{R}_c = \sin \psi \cdot R_{\oplus}$$

where \vec{n}^0 is the null vector of K , \vec{R}_c is the radius-vector of the segment middle and $R_{\oplus} = |\vec{R}_c|$ - the Earth radius. The radius-vector of the spherical segment centre \vec{R}_c can be presented in the following way:

$$(5) \quad \begin{cases} X_c = R_{\oplus} \sin \Theta \cdot \cos[\omega_{\oplus}(t - t_0)] \\ Y_c = R_{\oplus} \sin \Theta \cdot \sin[\omega_{\oplus}(t - t_0)] \\ Z_c = R_{\oplus} \cos \Theta \end{cases}$$

In (5) ω_{\oplus} is the Earth angular rotation velocity and t_0 is appropriately selected epoch (for example, the moment when the artificial earth satellite passes through the orbit perigee). If we substitute (5) in (4') we'll obtain:

$$(6) \quad A \cos \varphi + B \sin \varphi + C = 0,$$

where

$$A = n_x \cdot \sin \Theta, \quad B = n_y \cdot \sin \Theta, \quad C = \sin \psi - n_z \cdot \cos \Theta, \quad \varphi = \omega_{\oplus}(t - t_0).$$

By solving (6) we determine \vec{R}_c at the tangencing moments t_1 and t_2 as well as the very moments. Thus, for the tangent vector we can write down:

$$(7) \quad \vec{\tau} = (\vec{R}_c \times \vec{n}) \times \vec{n}$$

Vector $\vec{\tau}$ is determined in (7) in GeCS. We make a transformation of $\vec{\tau}$ in OCS [3]:

$$(8) \quad \vec{\tau}_{(OKS)} = \alpha_{OG_e} \cdot \vec{\tau}_{(GeKS)}$$

In (8) the transformation matrix α_{OG_e} has the following form [3]:

$$\begin{aligned} \alpha_{11} &= \cos \omega \cdot \cos \Omega - \sin \omega \cdot \cos i \cdot \cos \Omega \\ \alpha_{12} &= \cos \omega \cdot \sin \Omega + \sin \omega \cdot \cos i \cdot \cos \Omega \\ \alpha_{13} &= \sin \omega \cdot \sin i \end{aligned}$$

$$\begin{aligned}\alpha_{21} &= -\sin \omega \cdot \cos \Omega - \sin \omega \cdot \cos i \cdot \sin \Omega \\ \alpha_{22} &= -\sin \omega \cdot \sin \Omega + \sin \omega \cdot \cos i \cdot \cos \Omega \\ \alpha_{23} &= \cos \omega \cdot \sin i \\ \alpha_{31} &= \sin \Omega \cdot \sin i \\ \alpha_{32} &= -\cos \Omega \cdot \sin i \\ \alpha_{33} &= \cos i\end{aligned}$$

After determination of the tangent vector $\vec{\tau}$ in K , we can determine its crossing points with Kepler's ellipse in OCS:

$$(9) \quad \frac{(\xi+c)^2}{a^2} + \frac{\eta^2}{a^2(1-c^2)} = 1, \quad \eta = k \cdot \xi$$

In the second equation of system (9) k signifies the tangent's coefficient in OCS. The following relation exists between the orbital co-ordinates (ξ, η) and the eccentric anomaly E [1]:

$$(10) \quad \begin{cases} \xi = a (\cos E - c) \\ \eta = a \sqrt{1-c^2} \cdot \sin E \end{cases},$$

where a is the large orbital semi-axis, e - is the eccentricity. On the other side, on the basis of Kepler's equation we can write down:

$$(11) \quad t = t_0 + (E - e \cdot \sin E) / \lambda$$

After we find out the eccentric anomaly E in (10) and substitute it in (11), we determine the moments when the satellite crosses the specified tangents.

4. Estimation of the Method.

The explained method is analytical and it is presented by final formulae. It is reduced to a single application of the respective calculation procedure within the limits of one satellite circle. After correction of the orbital elements, the procedure can be repeated for the next interval of time. The examined method is based on a situational condition whose geometrical model is reduced to the determination of tangents $\vec{\tau}_1$ and $\vec{\tau}_2$ in GeCS. The transformation of the tangents in OCS is equivalent to the transformation of the situational condition in the orbital plane [6].

A structural approach is applied for the method algorithmization. Based on a programme complex for situational analysis, developed for solution of the problems in [6], it was necessary to add two new sub-programmes for ensuring the treated situational problem. This means that

the development of algorithms for situational analysis, based on the transformation of the situational conditions to Kepler's plane is facilitated by the presence of common sub-problems. In our case and for these in [6] this is the crossing of a straight line with Kepler's ellipse.

The following cases are possible for one Earth rotation around its axis:

- with sufficient orbital inclination equation (6) has four roots which leads to determination of four tangents connected with two crossings of segment S with Kepler's plane;
- with smaller orbital inclination equation (6) has two solutions which determine two tangents, corresponding to one crossing of segment S with K;
- with small orbital inclination segment S doesn't cross K.

The correction of the orbital elements of each satellite circle on the basis of the selected model of disturbances allows to apply the presented approach for situational analysis within long interval of time. Considering the effectiveness of the computation procedure, even for a long interval of time the computation expenses are much less than by verification along the orbit, performed with a step. The method is applicable in the cases when Kepler's approximation in the terms of the satellite's circle period is admissible with a view to the solved problem. For solving practical problems in many cases this is executed.

The offered method for determination of a satellite pass over a region of the earth surface, represented by a circular segment, as well as the examples, given in [6], are connected with a transformation of the situational condition in the plane of Kepler's orbit. Analogous to these examples, there are others, which allow to develop an analytical computation procedure, applicable within the terms of one period of the satellite circle. Such situational tasks, for example, are connected with a satellite pass through the shadow of the Earth, the Moon (a central body or its natural satellite). Analogous explanation can be made for the situational tasks for determination of a satellite pass through the impact wave, the magnetopause and the neutral layer, which are exceptionally important in the design of experiments of the type of INTERBALL [7].

References

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